

Evaluating Algae as an Alternative Fuel for Chemical Looping Combustion

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Abstract: Chemical Looping Combustion (CLC) and Chemical Looping with Oxygen Uncoupling (CLOU) are low-pollution energy generation techniques conventionally utilizing natural gas or synthetic gas as fuel. Using a redox reaction of metal oxides in dual fluidised beds, CO₂ can be captured and prevented from entering the atmosphere at efficiencies up to 80% [4,8]. Algae is a sustainable source of biofuel with the additional benefit of carbon capture through photosynthesis [7]. This Meta-Study attempts to determine the viability of algae as CLC/CLOU reactor fuel for long term sustainable energy generation by identifying trends in different fuels and reactants to see if algae fuel can produce an acceptable output and identify areas of weakness. Energy balance calculations were performed as well as thermal energy output, processing energy and enthalpy values. *Graciliara* sp. and *Chlorella Vulgaris* made the most effective fuels for CLC and CLOU respectively due to the low amount of algae required to produce fuel. For CLC, 3.57kg *Graciliara* sp. produced 1kg fuel. For CLOU, 1.7kg *Chlorella Vulgaris* produced 1kg fuel. CLOU was the most mass efficient with an energy/mass efficiency ratio of 11600kJ/kg compared to CLC's 15.7kJ/kg. The energy balance ratio analysis of the production of algal fuel also identified *Chlorella Vulgaris* as the best fuel, with an EBR of -0.4 in CLOU. In terms of evaluating output, CLOU's energy/mass efficiency ratio surpassed a modern coal plant [45], whose value was 2840 kJ/kg. The defining factor was the enthalpy of reaction.

Keywords: Chemical; Looping; Combustion; CLC; Algae; Biofuel; CSS



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1. Introduction

Concerns over global climate change and increasing pollution levels have led to increased effort into the research of renewable energy generation [13]. While most efforts have gone into the development of carbon neutral energy sources such as wind and solar power, carbon capture and carbon storage techniques for combustion-based generators are also being investigated [5,22,35,54]. Currently, three main processes are used to capture and store gaseous carbon dioxide that is generated during combustion. These include post-combustion, oxy-fuel combustion, and pre-combustion [36,37,38]. These processes, while efficient up to approximately 80% capture [4,8], (as seen in Fig. 1), require significant energy to initiate and sustain them.

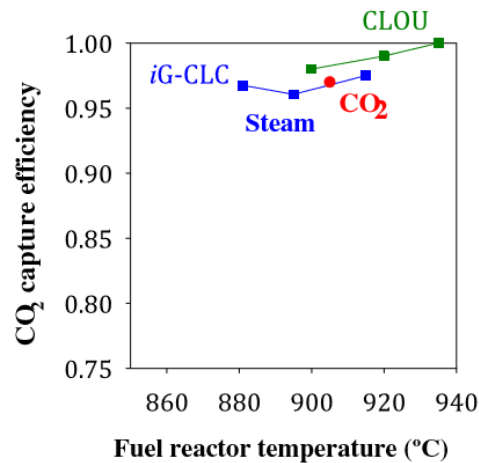


Figure 1. CO₂ capture efficiency vs fuel reactor temperature [8]

CLC is a flameless, cyclic energy generation and carbon capture technique that has been considered viable for mitigating the economic, environmental and energy costs of CO₂ capture and power generation [15,16,20]. The CLC process consists of two interconnected fluidized beds (layers of fluidized solid) and two main reactors [15,16,19]. An oxygen carrier, traditionally a metal oxide, reduces via combustion with a hydrocarbon fuel within the fuel reactor and is then sent to be re-oxidized in the air reactor before being sent to the fuel reactor. This cycle repeats continuously during the operation of the CLC system [17,21].

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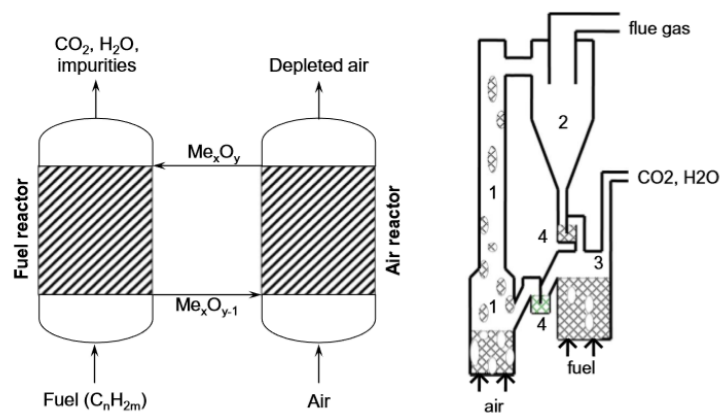
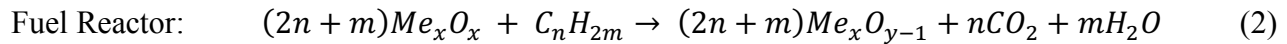
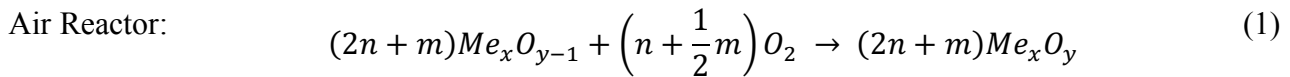


Figure 2. CLC process schematic [21]

The oxygen carrier is circulated between two fluidized beds, which eliminates the need for the fuel and air to be in contact with each other. Hence, the products of combustion (carbon dioxide

and water vapor) are not mixed with the rest of the fuel gases and almost pure carbon dioxide can be obtained [8]. This reaction cycle can be described by the chemical equations below:



The total amount of heat released from reactions (1) and (2) can readily reach enthalpies of 30kJ/g [53] (varying upon oxygen carrier) which is comparable to more traditional combustion techniques that require contact of fuel and oxygen, such as the regular atmospheric combustion of methane which produces 50kJ/g of heat [53].

Various CLC reactor types exist, the use of which is determined by the particular fuel used. Gaseous fuels such as natural gas or synthetic gas are combusted through the common CLC process [14,16]. Solid fuels are either directly combusted by the In-situ Gasification Chemical Looping Combustion (iG-CLC) or Chemical Looping with Oxygen Uncoupling (CLOU) process, or indirectly combusted through Syngas CLC [12,18,20]. The iG-CLC process works without a gasifier and therefore, no oxygen is required.

Solid fuel is mixed with the oxygen carrier which reacts with the gasification products of the fuel. Gasifying agents are then introduced into the fuel reactor to fluidise the fuel reactor [12,19]. The CLOU process involves segregation of the oxygen carrier so that gaseous oxygen is available for the combustion of the solid fuel. Once combustion occurs, the oxygen carrier is re-oxidised in the fuel reactor [26]. Combustion of liquid fuels is a new area for CLC technology and as of this point in time has been focused upon non-sulphurous fuels such as bitumen and asphalt [24]. Current research is being conducted upon the combustion of heavy fuels and vacuum residues [20].

Table 1. Comparison of various crops as a fuel source [8]

Crop	Oil Yield (L/ha)	Land Area required (M ha)	Existing US cropping area (%)
Corn	172	1540	846
Soybean	446	594	326
Canola	1190	223	122
Jatropha	1892	140	77
Coconut	2689	99	54
Oil Palm	5950	45	24
Microalgae ^a	136,900	2	1.1
Microalgae ^b	58,700	4.5	2.5

In recent years, sustainable alternatives to coal and oil have been explored [2,7,10,23,54], like solar power. While solar power enables sustainable power generation with little damage to the environment there are downfalls that hinder its widespread use. Previous studies in CLC have investigated fuels such as natural gas, coal and a variety of biomass such as pine saw dust [6]. In terms of CLC, the use of algal-based fuels in particular has potential [3]. The low CO₂ output of the reactor and CO₂ absorption of the algae may result a power system with net negative CO₂ output while maintaining a positive energy output.

As can be seen in Table 1. algae, particularly microalgae species, are promising sources of biofuels. Compared to other sources of biomass, oil yields for algae are greater per unit of land mass for fuel production [8]. However, oil yields and the compositions of the fuels produced from algae vary as there are several thousand different algae species [1,3]. Algae are eukaryotic organisms made mostly of chlorophyll which can be categorized by two main groups.

Macroalgae, also known as seaweeds which are multicellular organisms of macro-size (typically ranging from 0.5 – 60 meters in length) that live in marine environments such as seawater, wastewater [41,42]. The conversion of macroalgae to biogas can occur through various processes such as thermal treatment and fermentation, but the highest yield percentage is achieved through anaerobic digestion, which can produce up to 90% methane [42,44].

Microalgae are unicellular organisms of much smaller size (typically ranging from nanometers to millimeters in length) that can survive in extreme temperatures and with minimal water availability [41,42,43]. Macroalgae are usually considered for producing biogas which can yield up to 80% of the energy content of petroleum-based fuels, whilst microalgae species favor the production of biodiesel due to their high percentage of lipids compared to macroalgae [2,9,11,51].

The aim of this meta study is to evaluate various algae species for their use in CLC as well as to define key parameters for maximum efficient energy production.

2. Methods

Throughout this meta study 'Google Scholar', 'UTS online library', 'Scopus', 'ProQuest Science and Technology', 'Web of Science Core Collection' and 'Elsevier Science Direct' were used to find relevant articles. These databases were filtered using search terms 'Chemical Looping Combustion', 'Algae' and 'Biofuels' to identify original-research English language articles which had been published in a scientific journal. Desirable articles ideally focused on a thermodynamic aspect of the CLC Process, which could include, but was not limited to; the design and operating conditions of existing CLC systems for use in mathematical analysis, algae properties such as composition and oil yields that could affect calorific value or thermal energy calculations and thermodynamic values such as heat capacity for the calculations used in this study.

Potentially biased reports, such as those from environmental groups or private agencies, were examined and compared to unbiased technical documents from scientific research institutions. During the article and journal assessment period, all conflicts of interest between team members regarding the uncertainty of eligibility was resolved through discussion.

2.2 Data Processing

Table 2. Calculation parameters

Parameter	Symbol
Volumetric flow rate (L/min)	\dot{Q}_V
Fuel density (kg/L)	ρ_f
Mass flow rate (kg/s)	\dot{m}
Algal conversion factor (dimensionless)	ACF
Mass (biofuel) (kg)	m_b
Mass (algae input) (kg)	m_0
Mass (algae burnt) (kg)	m_f
Reactor Thermal output (W)	W_Q
Total energy output (J/24hr)	Q_{24hr}
Total energy output (Fuel Matched) (J/24hr)	Q_{m24hr}
Energy/Mass efficiency (J/kg)	η_m
Processing energy (J/kg)	E_p
Specific enthalpy (J/kg)	H
Power output	P_f
Power input	P_0

Algae types are listed, along with their fuel conversion ratios. Reactor properties such as reactor thermal energy output, fuel flow and pressure are collected. In the case of CLC, pressure is used to calculate the density of the gaseous fuel to determine the mass flow [49,50]. In the case of CLOU, since the fuel is solid, this step is not required as the mass flow is already in the correct unit.

$$\frac{(\dot{Q}_V \rho_f)}{60} = \dot{m} \quad (3)$$

The ratio of algae conversion into biofuel is taken from papers. This is used to determine the mass of algae required to produce 1 kg of fuel.

$$m_b = ACV \cdot m_0 \quad (4)$$

The outputs for the whole system over the course of 24 hrs (86400 seconds) are then simulated to determine which algae is the most effective for this reactor. This approach is taken to use time as the basis for measuring generation instead of mass used, which varies between each algae and therefore would lead to different operating times.

$$m_f = \dot{m} \cdot ACV \cdot 86400s \quad (5)$$

$$Q_{24hr} = W_Q \cdot 86400s \quad (6)$$

Table 3. Conversion ratio for different species of algae [35,43,45,46,47,48]

Algae	Conversion Ratio (kg Algae -> kg fuel)
Chlorella sorokiniana (CLOU)	4.54
Chlorella vulgaris (CLOU)	1.7
Dunaliella salina (CLOU)	2.27
Nannochloropsis oculata (CLOU)	3.37
Scenedesmus quadricauda (CLOU)	5.43
Tetraselmis suecica (CLOU)	4.35
Chaetoceros muelleri (CLOU)	2.98
Thalassiosira pseudonana (CLOU)	4.85
Ellipsoidion sp. (CLOU)	3.65
Ulva sp.1 (CLC)	6.66
Ulva sp.2 (CLC)	12.5
Ulva sp.3 (CLC)	5.2
Ulva sp.4 (CLC)	8.33
Ulva sp.5 (CLC)	6.66
Ascophyllum (CLC)	9.09
Laminara h (CLC)	4.35
Lamiara sacch (CLC)	4.54
Graciliaria sp. (CLC)	3.57
Sargassum fl. (CLC)	5.55

Note that a fuel processing energy cost can be determined by multiplying the denominator of this equation to simulate the energy requirements of transporting/converting the fuel. This changes the result into "Net Energy Output (J)"

$$Q_{24hr}(net) = \frac{Q_{24hr}}{E_p m_f} \quad (7)$$

The most important equation in this study is the one to determine the mass efficiency of the reactor- i.e. how much energy you get for how much fuel you burn. Since this is a ratio, it filters out the effects of order of magnitude and allows a valid comparison.

$$\eta_m = \frac{Q_{24hr}}{m_f} \quad (8)$$

To be effective, a reactor must at least approach the mass efficiency of commonly used plants and produce a comparable amount of power when scaled up to the same fuel input as commonly used plants. In this case, the plant used as a standard was a coal generator from the Heilbronn plant in Germany [43]. For these tests, the most effective algae for the CLC and CLOU cases were used. This is calculated to provide an easy way of showing the energy density of the fuels. While mass efficiency

avoids the issue of order of magnitude, since it is a ratio, total energy output must be determined differently. The fuel flows of each reactor were adjusted to match the value of the coal generator and the energy output recalculated:

$$Q_{m24hr} = E_p \frac{\dot{m}_{Heilbronn}}{\dot{m}} \quad (9)$$

Specific Enthalpy due to algae mass was calculated from the enthalpy of reaction using standard tables and Sabatier's reaction for methane. Solid fuel specific enthalpy couldn't be calculated due to complexity and lack of available data:

$$H = \frac{H_r}{m} \quad (10)$$

Energy Balance Ratios were calculated based off production cost assumptions from [32], where two conditions for raceway ponds and PBRs were presented. For the raceway ponds the base case gave one watt per 10 grams of algae produced for power input and the maximum case gave one watt per twenty grams. PBRs had a base case of 500 watts per twenty grams of algae produced and the maximum case gave 50 watts per 40 grams produced. This was then factored and multiplied by our calculated mass of algae required to power a 10 kW and 1.5 kW CLC. The ratio was then calculated:

$$\frac{P_f - P_i}{P_i} \quad (11)$$

3. Results and Discussion

3.1. Generator fuel/type compared to mass efficiency

Though the CLC reactor types follow the same basic principles, the various ways in which different CLC fuels are treated can affect the overall energy produced per mass of the fuel. Table 4 illustrates the effect the various CLC processes would have upon the treatment of various algae fuels.

For the CLC labelled values, it is assumed that the algae has been converted to methane prior to combustion within a conventional CLC reactor. The assumption is only made for the purposes of accurately comparing the CLC reactor's performance, as this is not a measurement of net energy- only thermal energy output per the mass of the algae. For the CLOU values it is assumed that a solid fuel biomass is used in the fuel reactor and that the main constituent for combustion is the lipid content of the material.

It appears that CLOU processing of algae biomass provides a comparable energy output to coal. However, the lipid content of the algae only amounts to 20-30% of its dry weight on average, so much of it is turned into waste products during combustion [34]. Comparatively, algae that has been converted to either gaseous or liquid fuels produces very little waste product after combustion. Though these results would indicate that the CLOU is best for mass efficiency, it is worth noting that the various treatments and production process to produce the type of algae fuel required can vary greatly.

Table 4. The amount of thermal energy produced in 24 hours per kilogram of fuel in each instance [35,43,45,46,47,48,52]

Generator	Thermal Energy per Kg material burnt (kJ/kg)
Heilbronn coal plant	2840
Tri-generator-LPG	3.48
Graciliaria sp.(CLC)	15.7
Ulva sp.1 (CLC)	8.44
Ulva sp.2 (CLC)	4.49
Ulva sp.3 (CLC)	10.8
Ulva sp.4 (CLC)	6.74
Ulva sp.5 (CLC)	8.44
Ascophyllum (CLC)	6.18
Laminara h (CLC)	12.9
Lamiara sacch (CLC)	12.4
Sargassum fl. (CLC)	10.1
Chlorella sorokiniana (CLOU)	4330
Chlorella vulgaris (CLOU)	11600
Dunaliella salina (CLOU)	8650
Nannochloropsis oculata (CLOU)	5830
Scenedesmus quadricauda (CLOU)	3620
Tetraselmis suecica (CLOU)	4510
Chaetoceros muelleri (CLOU)	6590
Thalassiosira pseudonana (CLOU)	4050

Thermal Energy per Kg material (kJ/kg) vs. Fuel Type

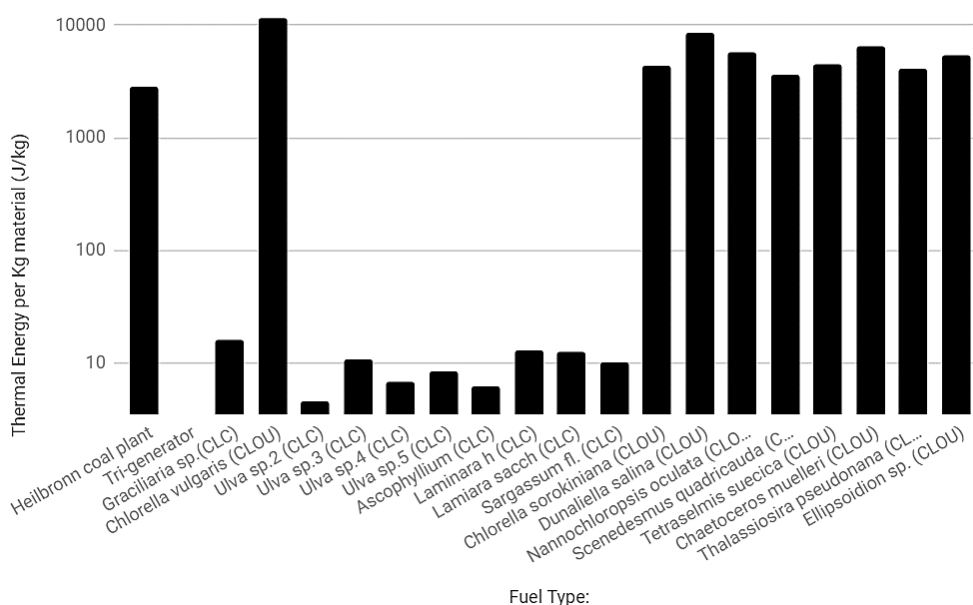


Figure 3. Thermal Energy per Kg material vs Fuel Type (including coal generator [35,43,45,46,47,48,52])

3.2. Generator Type at Equal Fuel Flow/Energy Density

Table 5. Fuel flow vs reactor type [35,43,45,46] for the purpose of reference/comparison to following graph.

Reactor Type	Heilbronn	GRACE CLC	CLOU	Tri-generator
Fuel Flow (kg/h)	5.66E+07	1.54E+04	2.20E-01	5.52E+02

The fuel flows in each reactor are of different orders of magnitude. When they are equalized, the energy outputs correlate to the mass efficiency, suggesting the reaction method - as opposed to reactor scale – is the defining factor in the mass efficiency of the reactor. Fuel type is also not the defining factor, as from Table 3 the conversion factors for the CLC and CLOU algae used were 3.57 and 1.7 respectively. This difference of scale- roughly 2 times – would not equalize the outputs of each reactor.

Fuel Flow Equivalent (Heilbronn) 24 Hr Energy Output (TJ) vs. Reactor Type

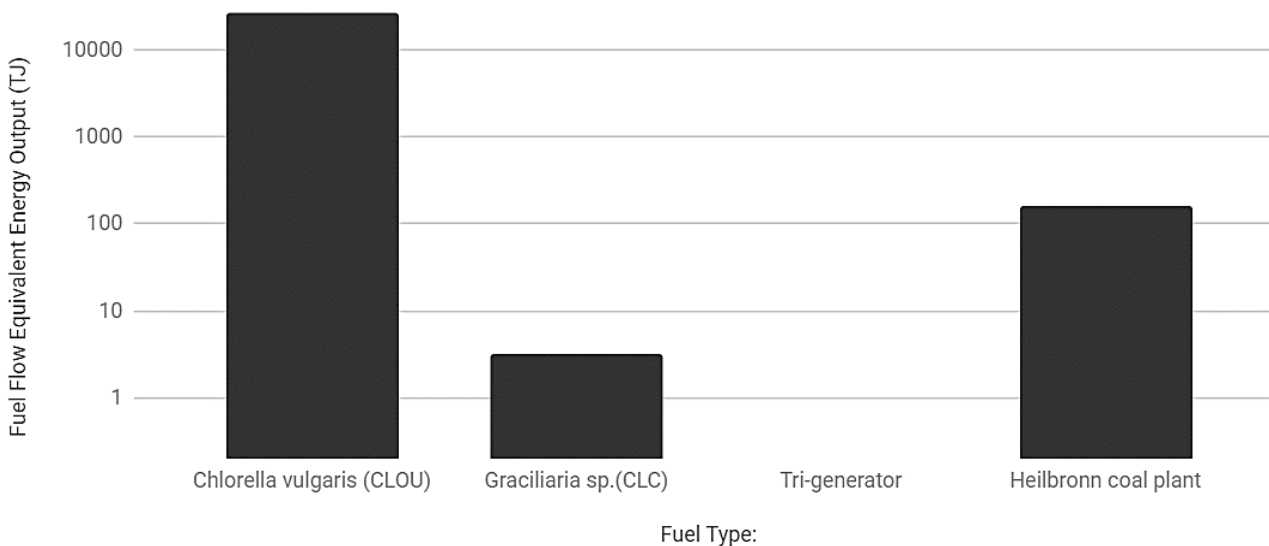


Figure 4. Fuel flow equivalent 24 Hr energy outputs for equivalent to Heilbronn fuel flow [35,43,45,46,47,48]

3.3. The effect of higher fuel processing energies on the net output of generators

The lower the mass efficiency of the generator, the quicker the net energy becomes a negative given a range of processing energies. These results were derived from the mathematical method described in equation (7). Coal and CLOU require immense amounts of energy to be used in their processing for their outputs to become negative, whereas CLC fades early.

Table 6. Algae species selected for use in this table made the most effective fuel for their respective generators. This table uses values of mass efficiency derived from equation (8) [35,43,45,46,47,48]

Processing energy (J/kg)	CLC (Grac. sp.)	Heilbronn Plant	CLOU (Chlor. Vul)
	η_m (kJ/kg)	η_m (kJ/kg)	η_m (kJ/kg)
1	15.7	2840	11600
5	3.15	568	2310
10	1.57	284	1160
50	0.315	56.8	231
100	0.157	28.4	116
500	0.032	5.68	23.1
1000	0.016	2.84	11.6
5000	0.003	0.568	2.31

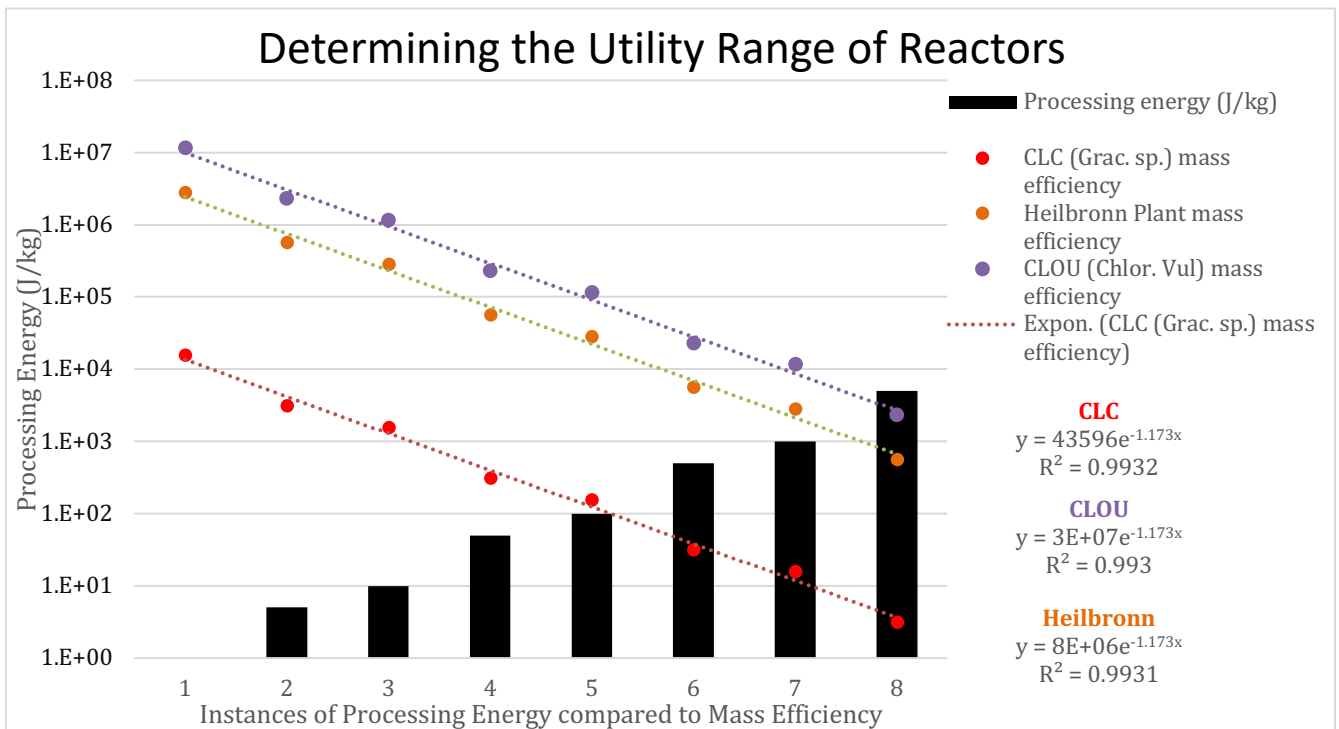


Figure 5. Fuel flow equivalent 24 Hr energy outputs for equivalent to Heilbronn fuel flow [35,43,45,46,47,48]

3.4. Enthalpy/Calorific Value/Algae Properties

Enthalpy determines the amount of heat that is released upon combustion of a fuel. Of the algae species studied above Graciliaria has the highest specific enthalpy for algae species converted to methane. In the below figure, Graciliaria sp. has a higher carbohydrate and protein composition than the Ulva species which would indicate that the higher these values are, the greater the specific enthalpy of the fuel.

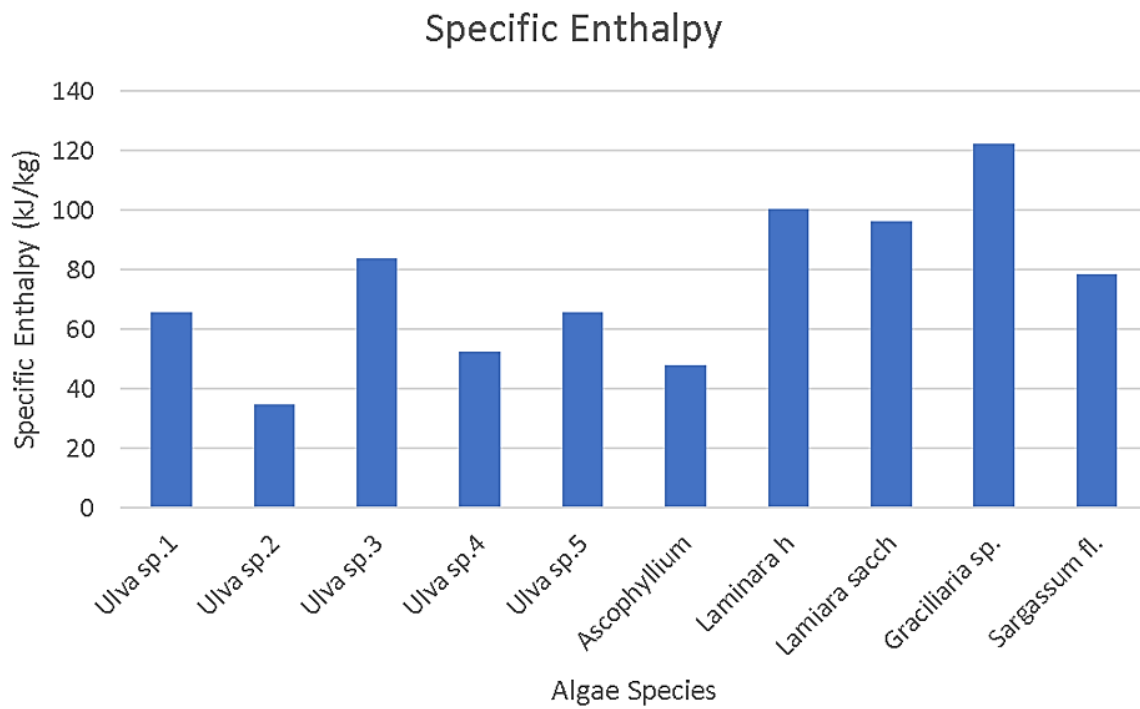


Figure 6. Specific enthalpy by algae species [1,2,3,7,10,11]

Enthalpy determines the amount of heat that is released upon combustion of a fuel. Of the algae species studied above Graciliaria has the highest specific enthalpy for algae species converted to methane. In the below figure, Graciliaria sp. has a higher carbohydrate and protein composition than the Ulva species which would indicate that the higher these values are, the greater the specific enthalpy of the fuel.

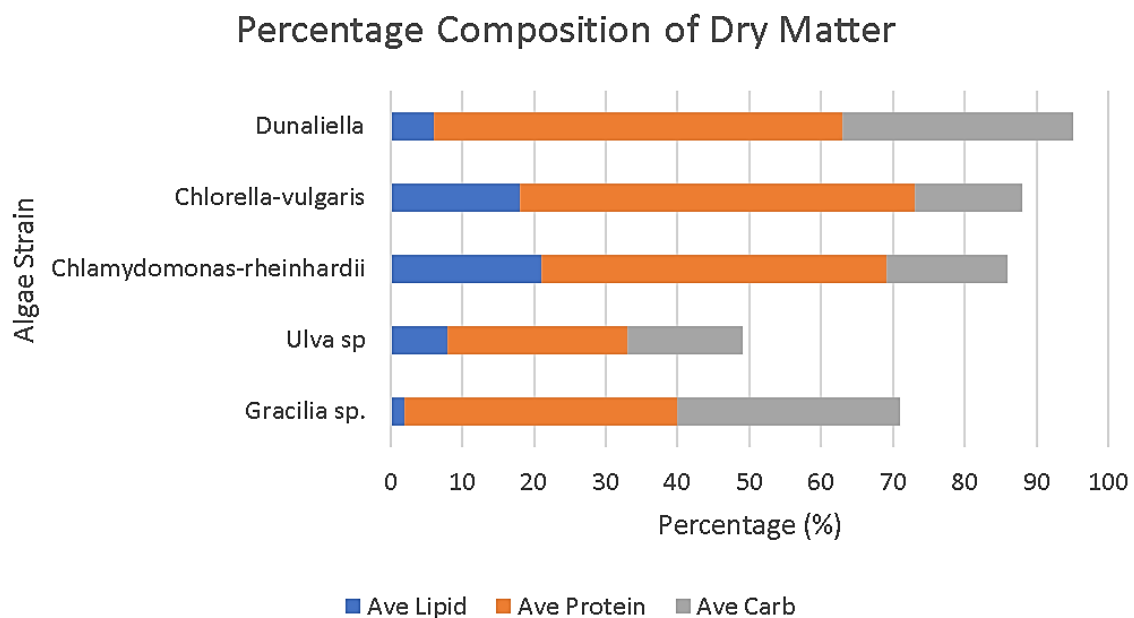


Figure 7. Chemical composition of microalgal species from [32,33,37,47,48,52]. Results are expressed as percentage of dry wt. Biomass.

Algae species vary by their lipid, carbohydrate and protein compositions. Current studies show that high lipid and carbohydrate concentration contributes to calorific value, the amount of polysaccharides

produced per species can be converted into bioethanol and available triacyl glycerides can be converted to biodiesel [27].

As in 3.3, the calorific value of algae compared to coal is quite low and there is much variation between algae species as well as the production processes used to cultivate algae. Current research into algae as a source for biofuel is concentrated around increasing this calorific value.

Chia et al, found that varying the concentration of phosphorus found in the *Chlorella vulgaris* strain increased its calorific value from 13.48 kJ/g up to 33.07 kJ/g [27]. R Slade et al, compared the various algae cultivation techniques and found that by comparing the Net energy ratio (as a measure of the energy needed to produce algae and the energy content of the algae) of algae grown through different processes, they were able to identify that Raceway Ponds are the best setups for a positive energy balance over PBR systems [32].

3.5. Energy to cultivate algae vs. Energy Output

For the following graphs and tables the generator output was taken from the 10 kW CLC and 1.5 kW CLOU models. The mass was divided by Biomass productivity [32] to find the power required to make the 10 kW energy for the day. Here, the Energy Balance Ratio is defined as the power required to produce n amount of algae for one day over the power output. This is calculated for Raceway ponds and Photo Bio Reactor systems.

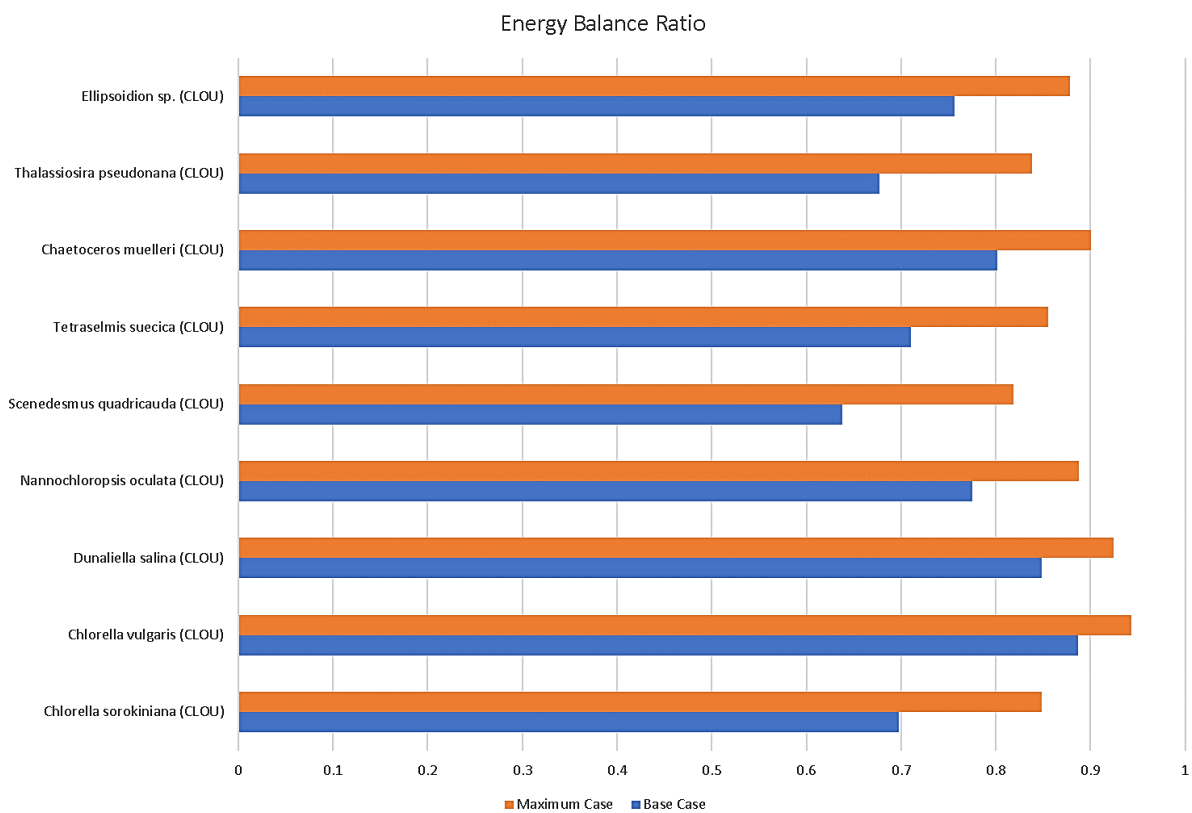


Figure 8. Energy balance ratio with CLOU reactor [32]. The blue lines indicate the use of a standard Raceway Pond setup. The orange lines indicate the use of an improved Raceway Pond [32].

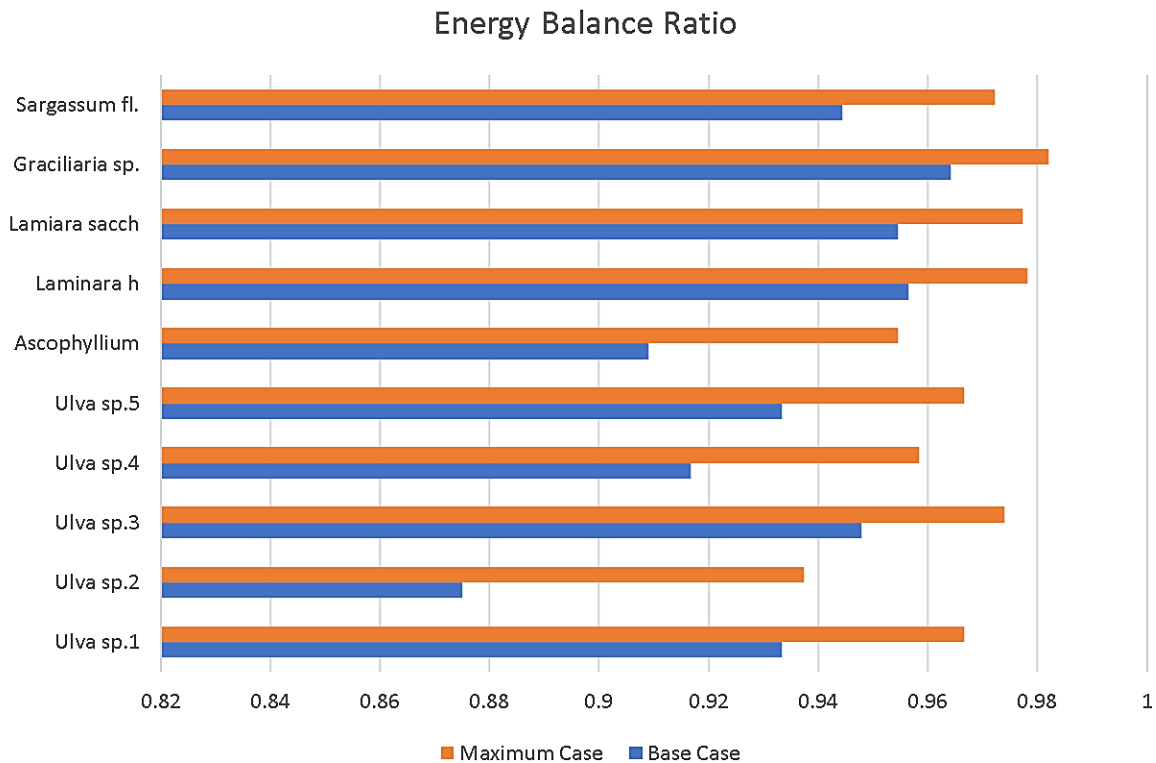


Figure 9. Energy balance ratio in CLC reactor [32]. The blue lines indicate the use of a standard Raceway Pond setup. The orange lines indicate the use of an improved Raceway Pond [32].

Raceway Ponds appear to be an ideal production process of algae for CLC. For the 1.5 kW CLOU model, the energy balance ratio calculated for power input over power output ranged from 0.64 for *Scenedesmus quadricauda* to 0.89 for *Chlorella Vulgaris*. This range was based on common raceway pond designs. For most efficient Raceway Pond design [32], the energy balance ratio ranged from 0.82 to 0.94 for the same species.

For the 10 kW CLC model, the energy balance ratio calculated for power input over power output ranged from 0.88 for *Ulva sp.2* to 0.86 for *Graciliaria sp.* in the base case. For the most efficient raceway pond design studied in [32], the energy balance ratio ranged from 0.94 to 0.98 for the same species.

The Photobioreactor (PBR) results, in comparison, were quite poor. For the 1.5 kW CLOU model, the energy balance ratio for PBR ranged from -79.8 for *Thalassiosira pseudonana* to -27.3 for *Chlorella Vulgaris*. For the most efficient PBR design, the energy balance ratio ranged from -0.4 to -3.0 for the same species. This presents a drastic improvement as a result of better PBR system designs. However, the negative values still indicate that more energy is input than output and this is not ideal.

The same trend was observed in the 10kW CLC model, with a marked increase in improvement from the basic PBR design to an improved one. The energy balance ratio ranged from -30.3 for *Ulva sp 2.* to -7.9 for *Graciliaria sp.* in the base case. For the most efficient PBR design, the energy balance ratio ranged from -0.6 to 0.6 for the same species. Though improvements in PBR design greatly improve the EBR, the Raceway Pond method of cultivation for algae have the best EBR values overall. The best algae source from those studied is *Chlorella Vulgaris*.

Table 7. CLOU energy balance ratio for algae with PBR reactor [32]. Any value in the negative indicates more energy is put in than is received.

Algae	EBR (Base)	EBR (Maximum)
Chlorella sorokiniana	-74.7	-2.8
Chlorella vulgaris	-27.33	-0.4
Dunaliella salina	-36.8	-0.9
Nannochloropsis oculata	-55.2	-1.8
Scenedesmus quadricauda	-89.5	-3.5
Tetraselmis suecica	-71.5	-2.6
Chaetoceros muelleri	-48.7	-1.5
Thalassiosira pseudonana	-79.8	-3.0
Ellipsoidion sp.	-59.8	-2.0

Table 8. CLC energy balance ratio for algae with PBR reactor [32]. Any value in the negative indicates more energy is put in than is received.

Algae	EBR (Base)	EBR (Maximum)
Ulva sp.1	-15.7	0.2
Ulva sp.2	-30.3	-0.6
Ulva sp.3	-12.0	0.4
Ulva sp.4	-19.8	0
Ulva sp.5	-15.7	0.2
Ascophyllum	-21.7	-0.1
Laminara h	-9.9	0,5
Lamiara sacch	-10.4	0.4
Graciliaria sp.	-7.9	0.6
Sargassum fl.	-12.9	0.3

4. Conclusions

A mathematical model was produced to calculate the net output energy of biofuels in a CLC reactor produced from a range of algae. It was found that the most suitable candidate for CLC was Graciliaria sp from the amount of methane able to be converted from the biomass, with 3.57kg algae being used to form 1kg methane. Likewise, for CLOU the most suitable candidate was Chlorella Vulgaris for the same reason, with a conversion factor of 1.7kg->1kg.

The use of improved raceway ponds to breed algae could improve the energy balance ratio; resulting in an increase of efficiency, with EBR increases of 0.18-0.05 in CLOU reactors and 0.06-0.02 in CLC reactors.

Even though in CLOU much of the algae is discarded before combustion, potentially requiring a lot of energy and wasting a lot of mass, the outputs pay off due to its enthalpy of combustion. It has a mass efficiency of 11600kJ/kg, much more effective than the coal plant, with a value of 2840kJ/kg. When the energy required to process the algae rises, CLOU's net energy only drops to negative at 5kJ/kg fuel / 2.31kJ/kg mass efficiency- at the same level, the coal generator's energy is 5kJ/kg fuel / 0.568 kJ/kg mass efficiency. CLC drops off at 0.5kJ/kg fuel / 0.032kJ/kg mass efficiency. Even over

a wide variety of fuels, each reaction type stayed within the same order of magnitude- there was not a single instance where a fuel variance raised the abilities of one reactor over another. The defining factor for a successful reactor is therefore enthalpy of combustion over all other factors including both fuel type and reactor size/fuel flow, and an algae-powered CLOU excels at it.

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